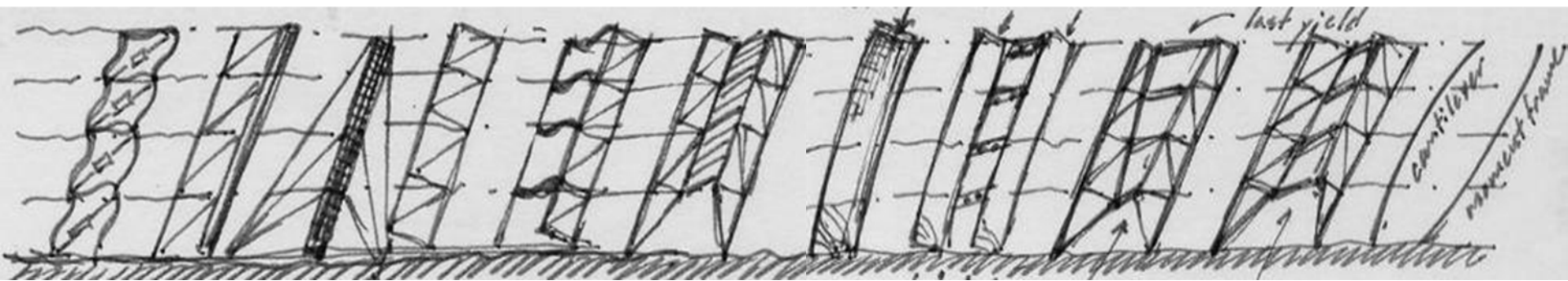


design choices are

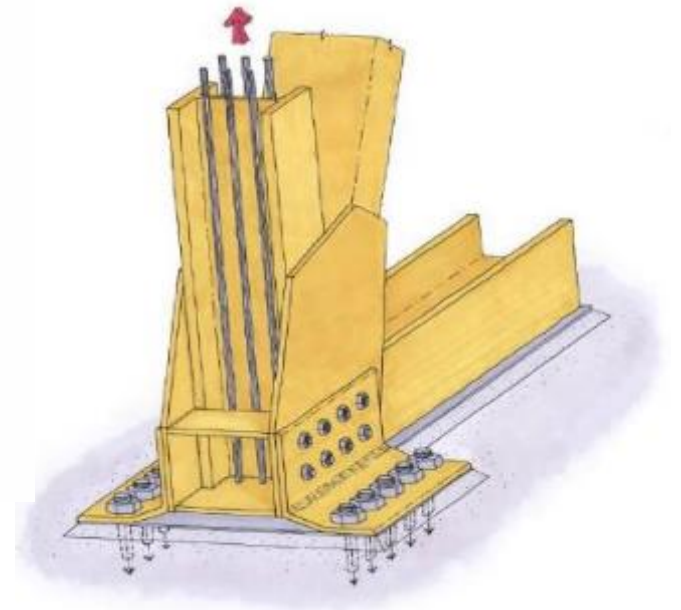
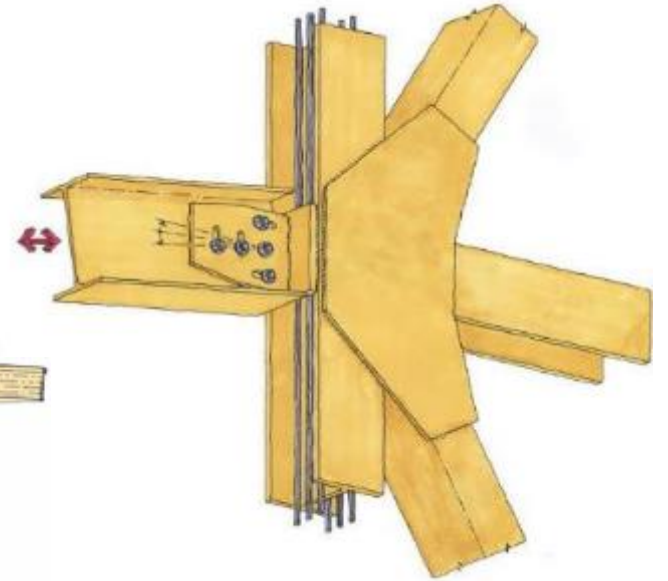
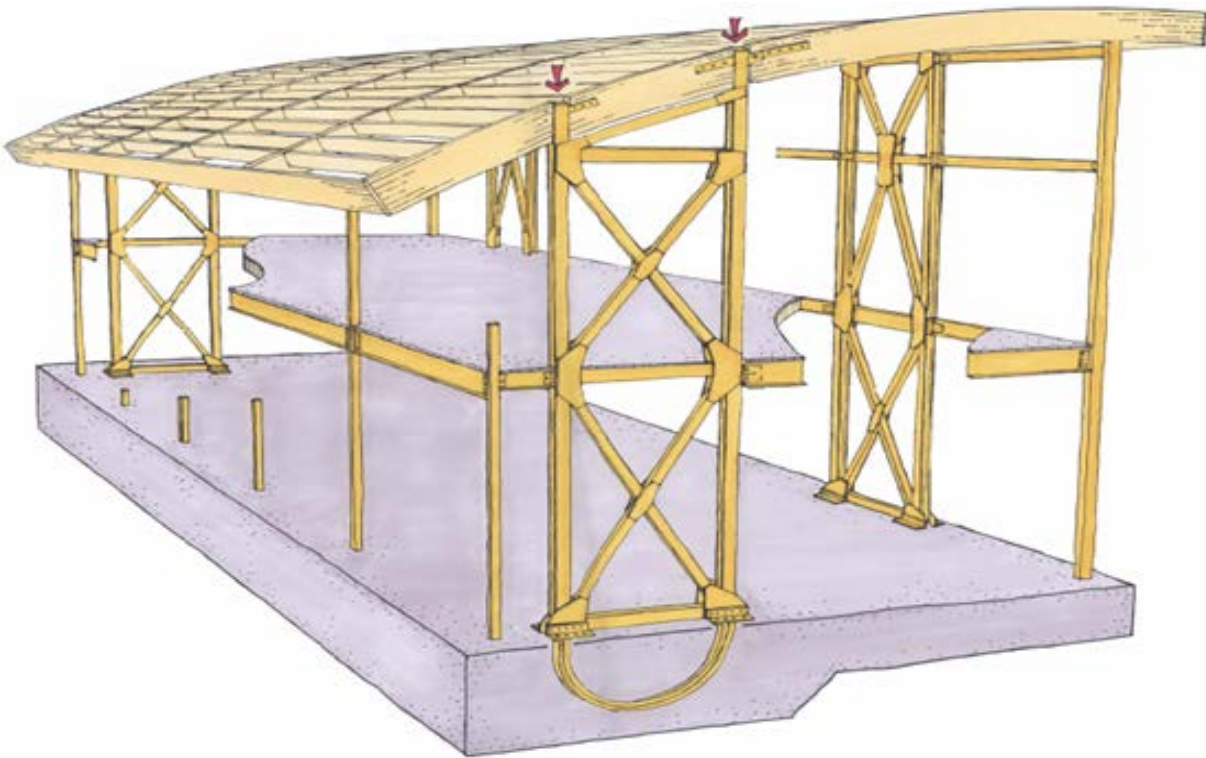


**P e r f o r m a n c e   I n v e s t m e n t s**

# Orinda City Offices, Orinda

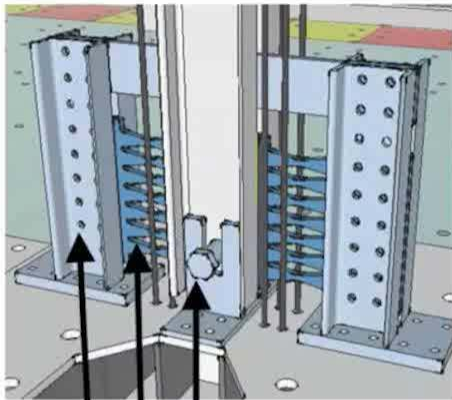
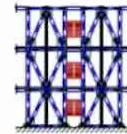
Architect: Siegel and Strain







# TEST A1 CONFIGURATION



Pin Moves Center of Fuse Up and Down

Fuse is Steel Plate with Specially Designed Cutouts

Small Frame Restrains Motion of Sides of Fuse

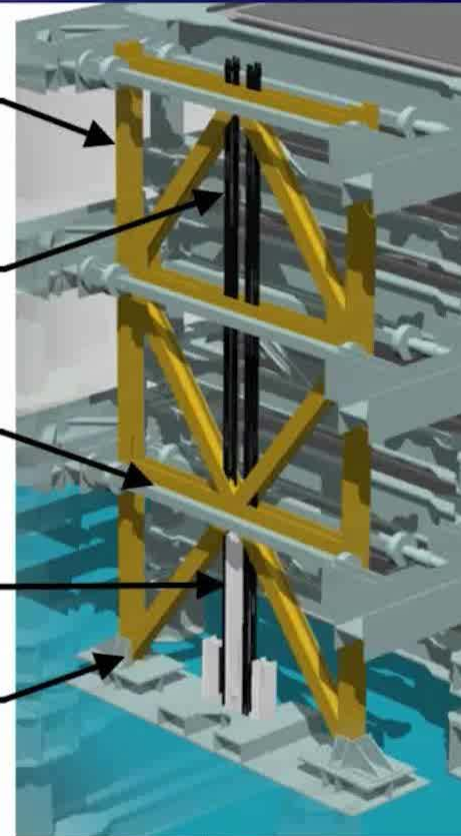
Steel Frame Remains Essentially Elastic, but is Allowed to Rock at the Base

Post-Tensioning Strands Bring Frame Back to Center After Shaking Stops

Pinned Struts Transfer Load to the Frame but Allow Uplift

Center Column Connects Frame to Fuse

Base of Frame is Free to Uplift

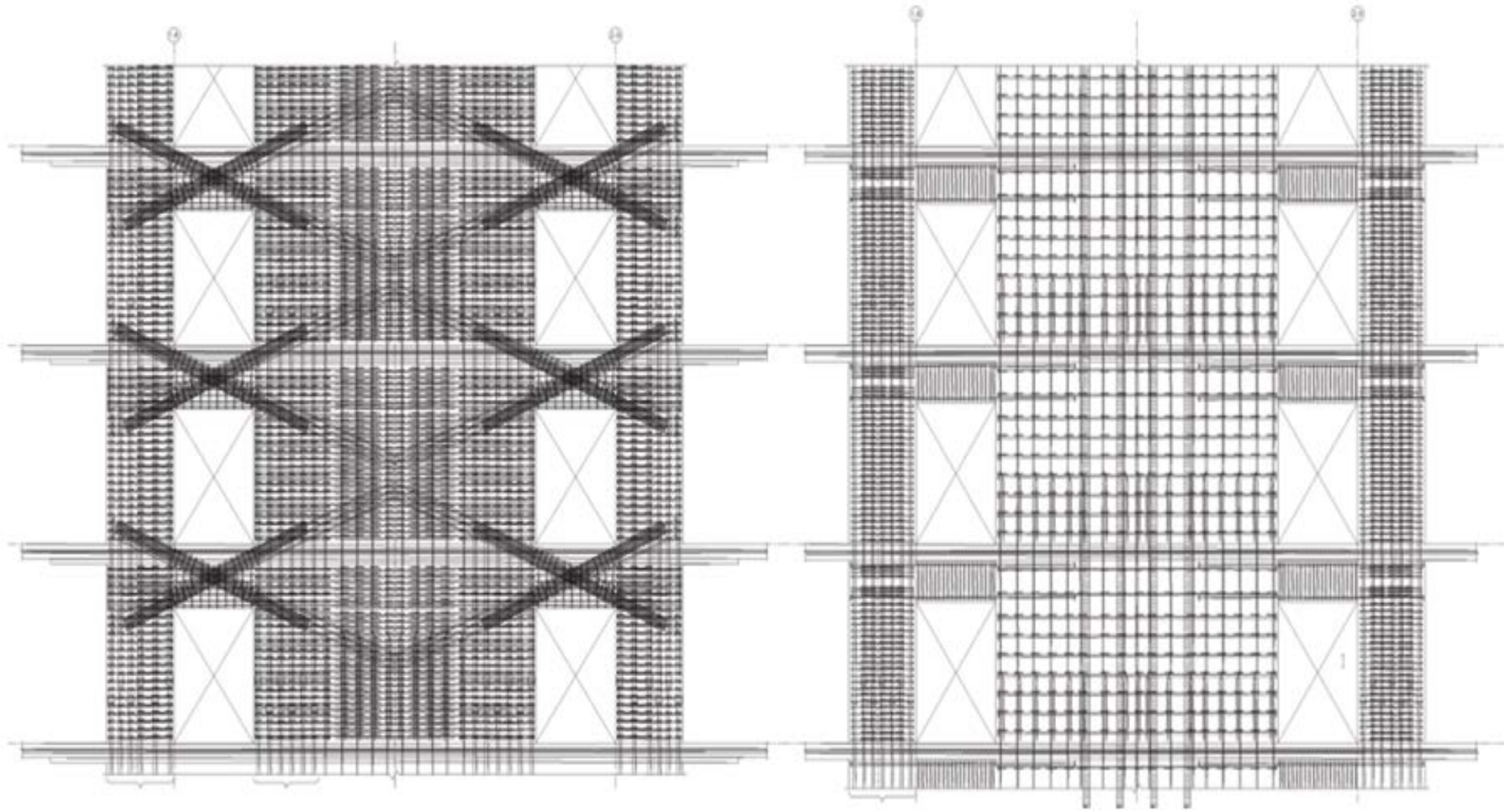


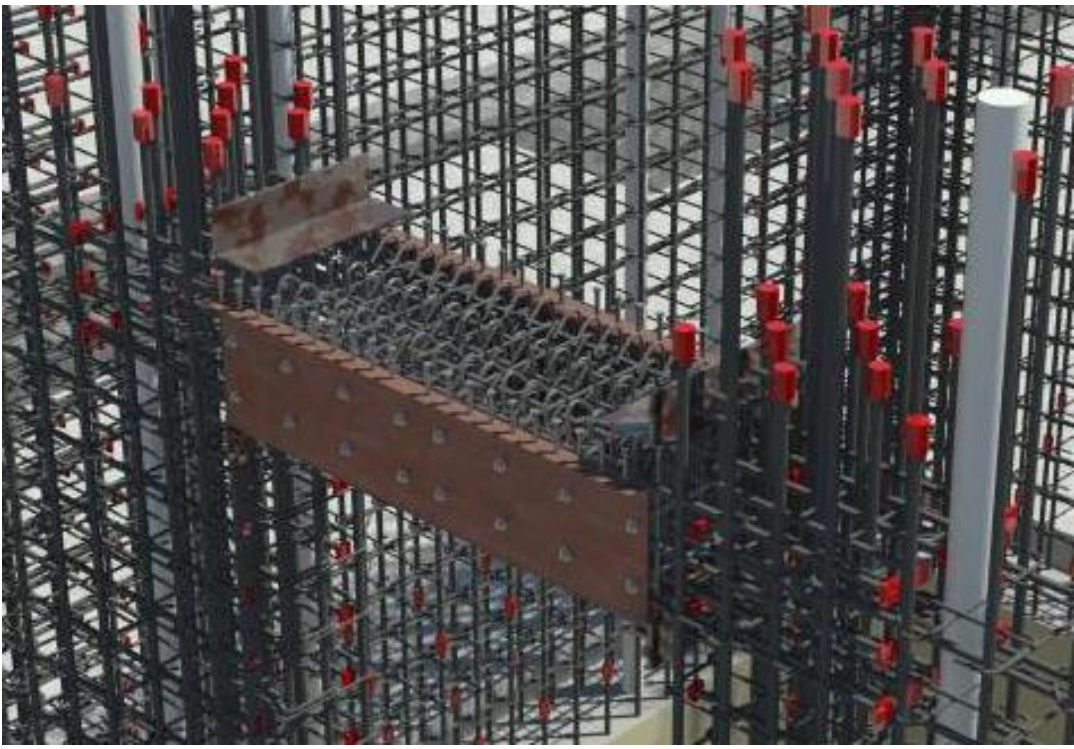
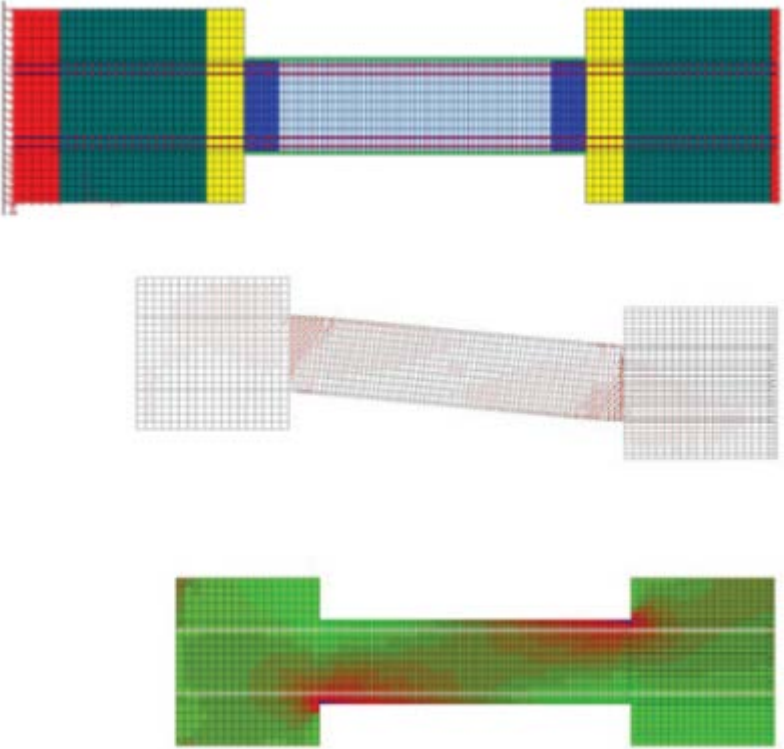
# SF Public Utilities HQ, SF

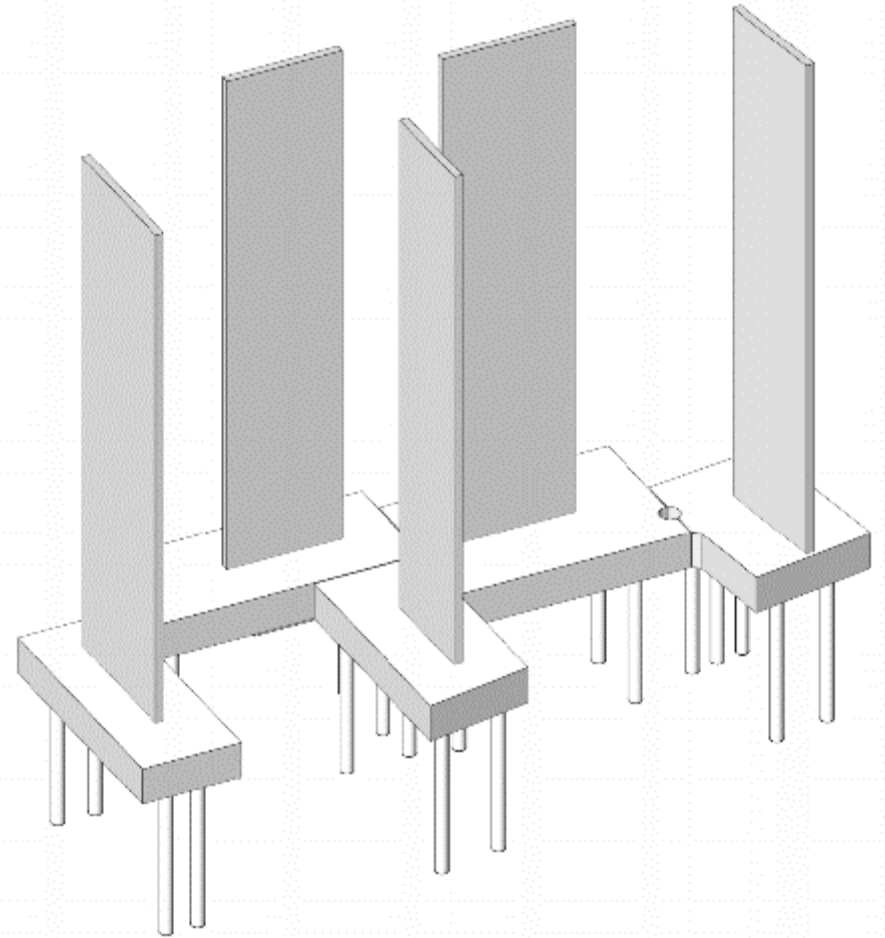
Architect: KMD/Stevens







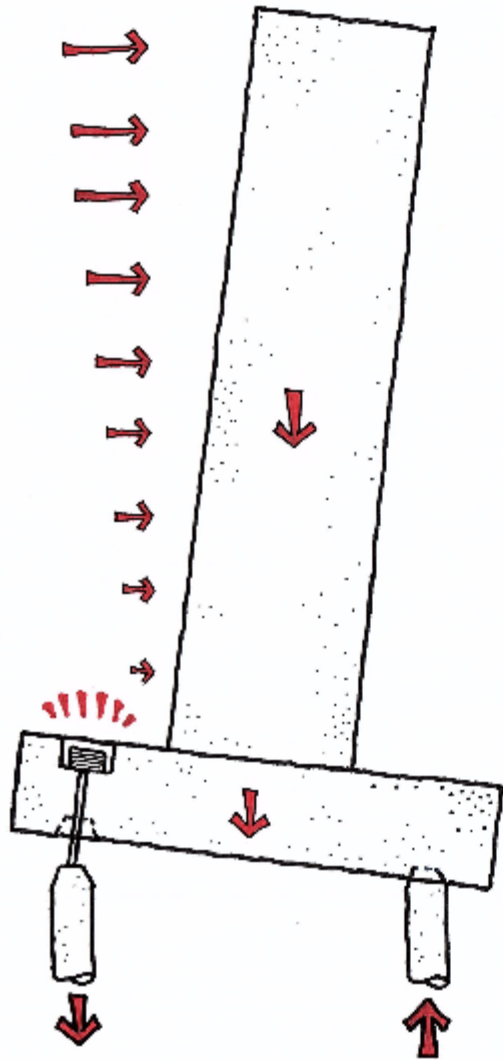




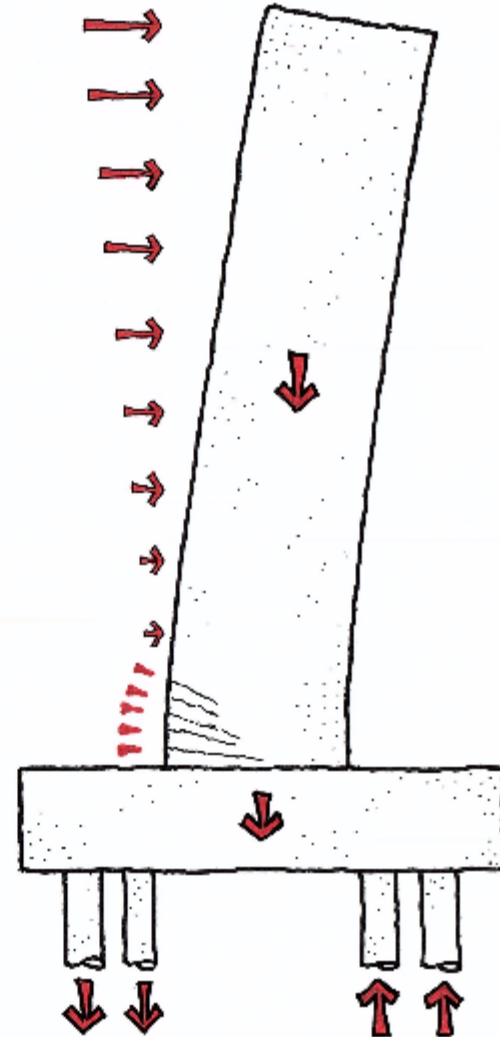
**1296 Shotwell St, SF**  
*Architect: Herman Coliver Locus*

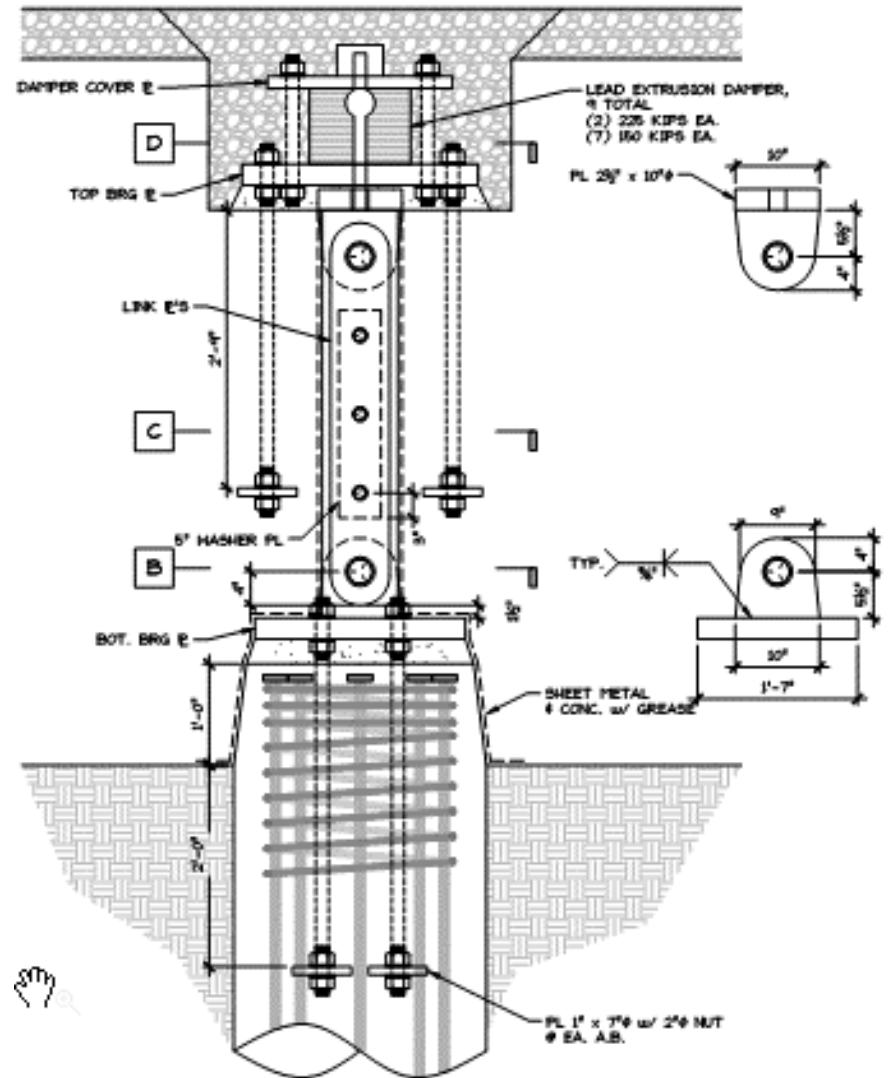
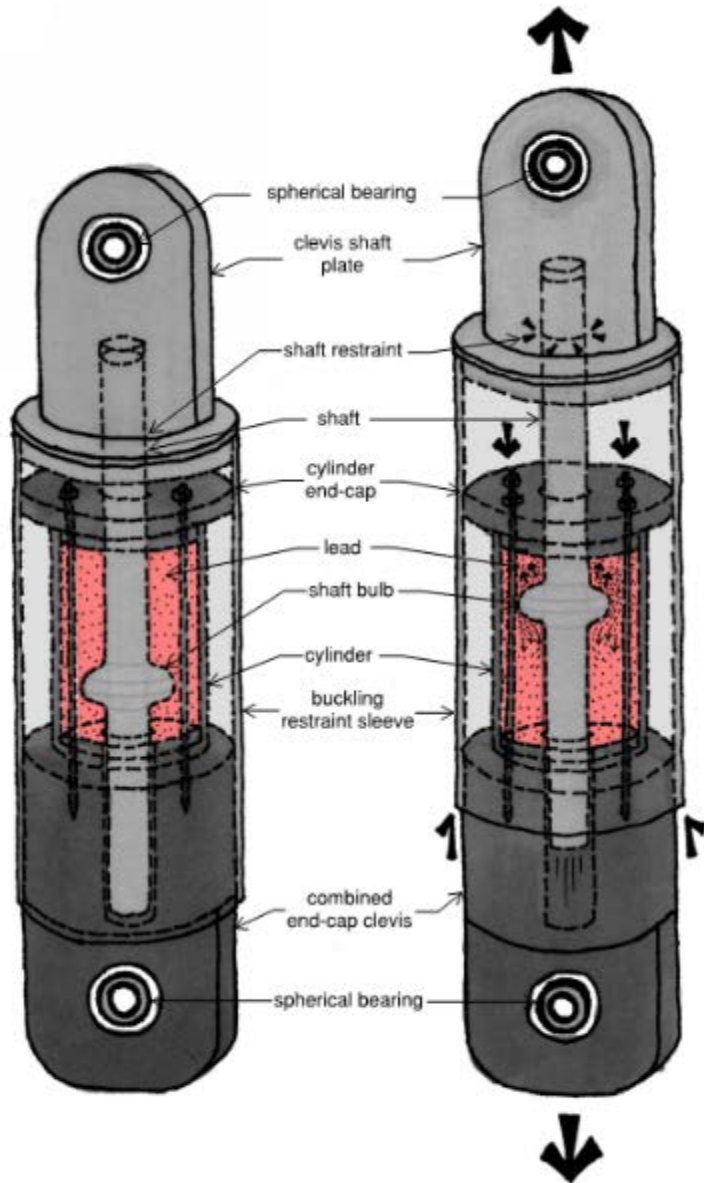


Performance Based Design

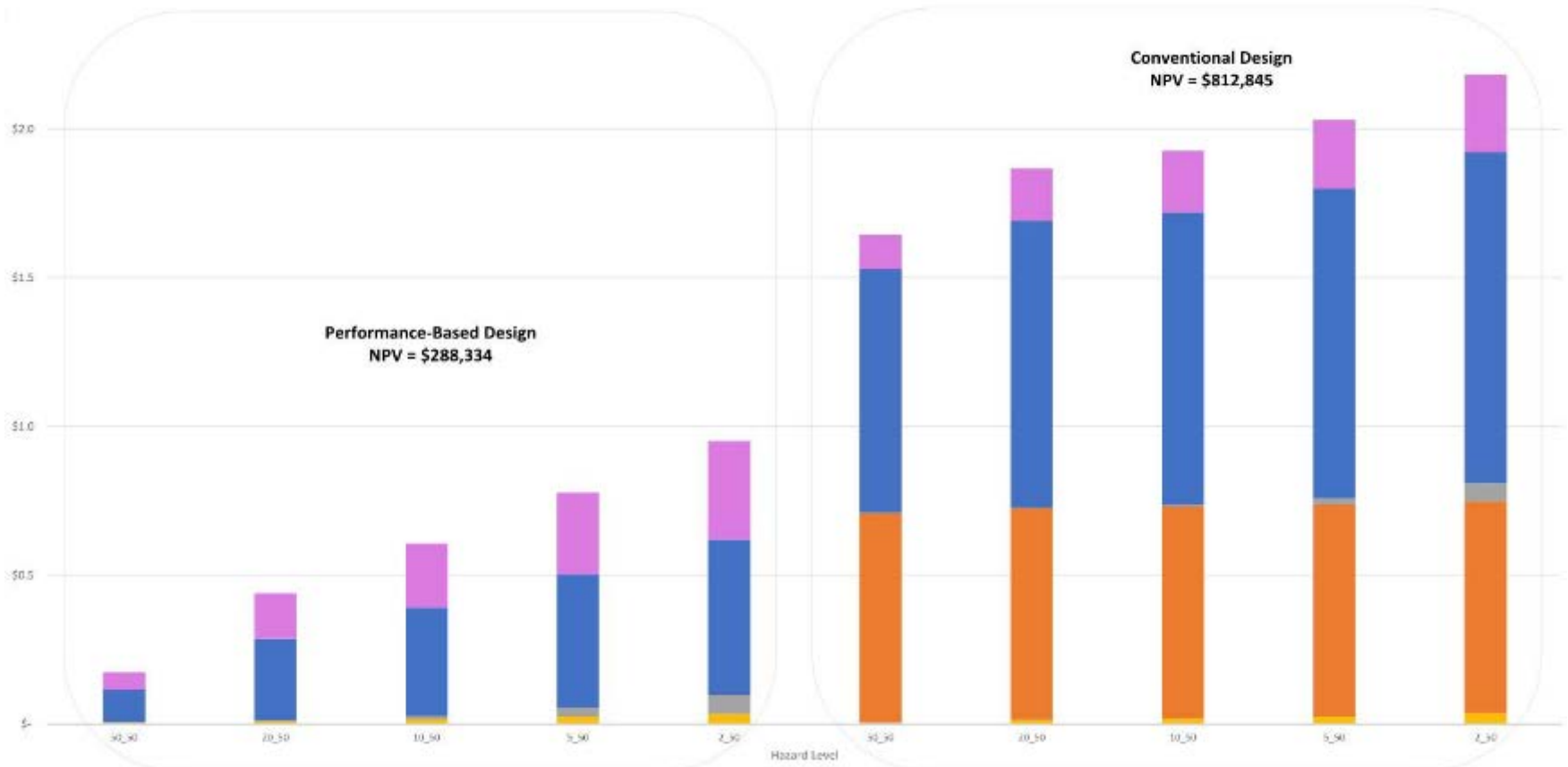


Conventional Design





- Partitions
- Stucco Skin
- Glazing
- Structure
- Plumbing and HVAC



## Economic Loss Modeling, FEMA P58 and SP3



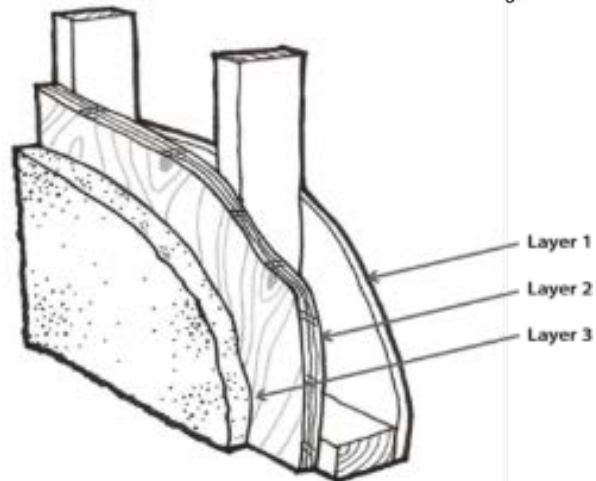
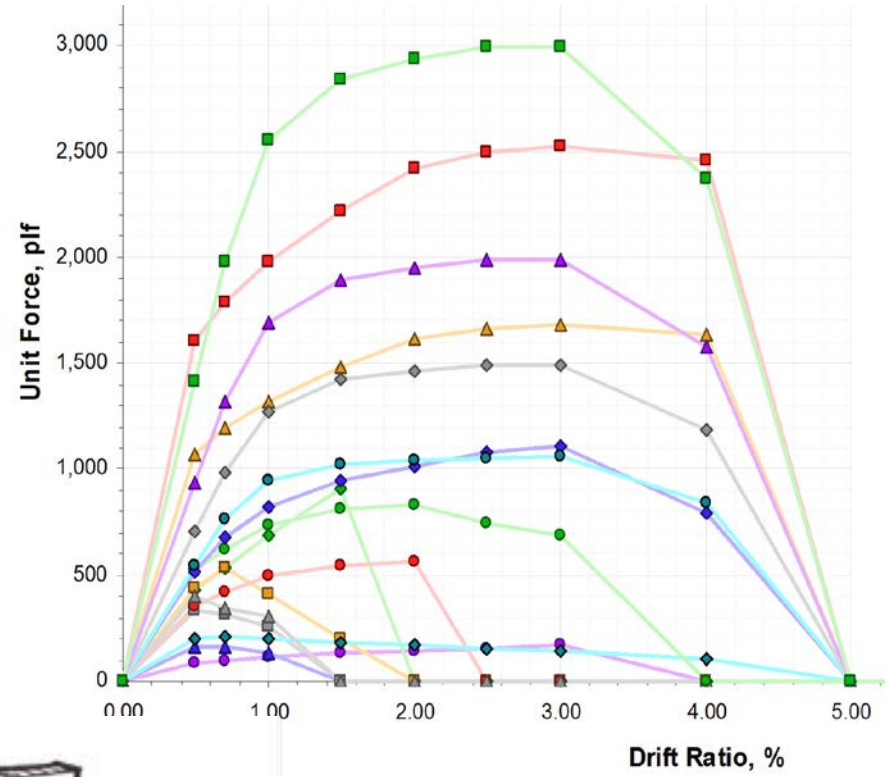
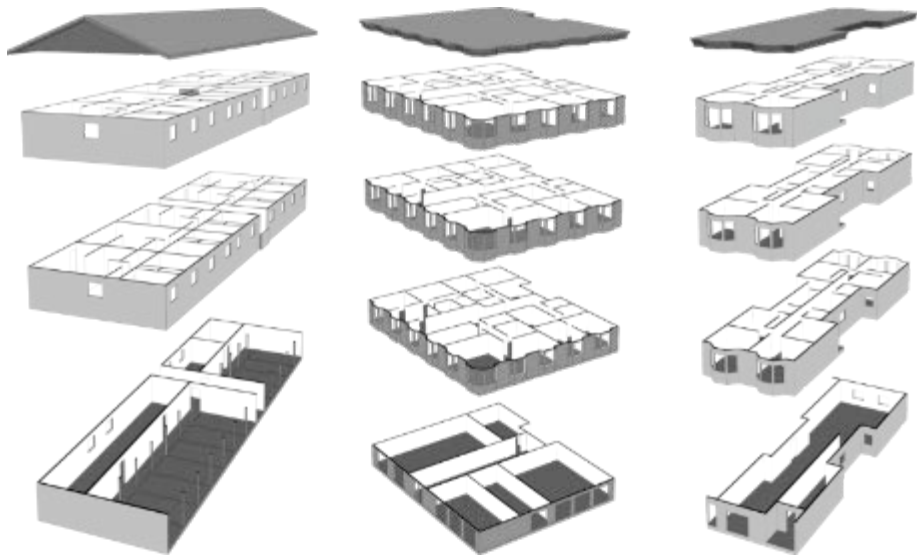




## F E M A P 8 0 7

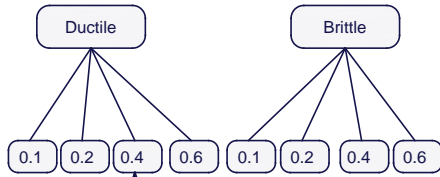
Seismic Evaluation and Retrofit of Multi-Unit Wood-Frame Buildings With Weak First Stories





# Surrogate Structures

Material forms:  
(2) total



Upper-story strength ratios,  $A_u$ :  
(4) per mat'l form

Weak-story ratios,  $A_w$ :  
0.6 to 1.1 by 0.1  
(6) per upper-story strength

Retrofit strengths:  
 $A_w$  to 1.6  
(51) per upper-story strength ratio

TOTAL NUMBER OF BUILDINGS:  
612

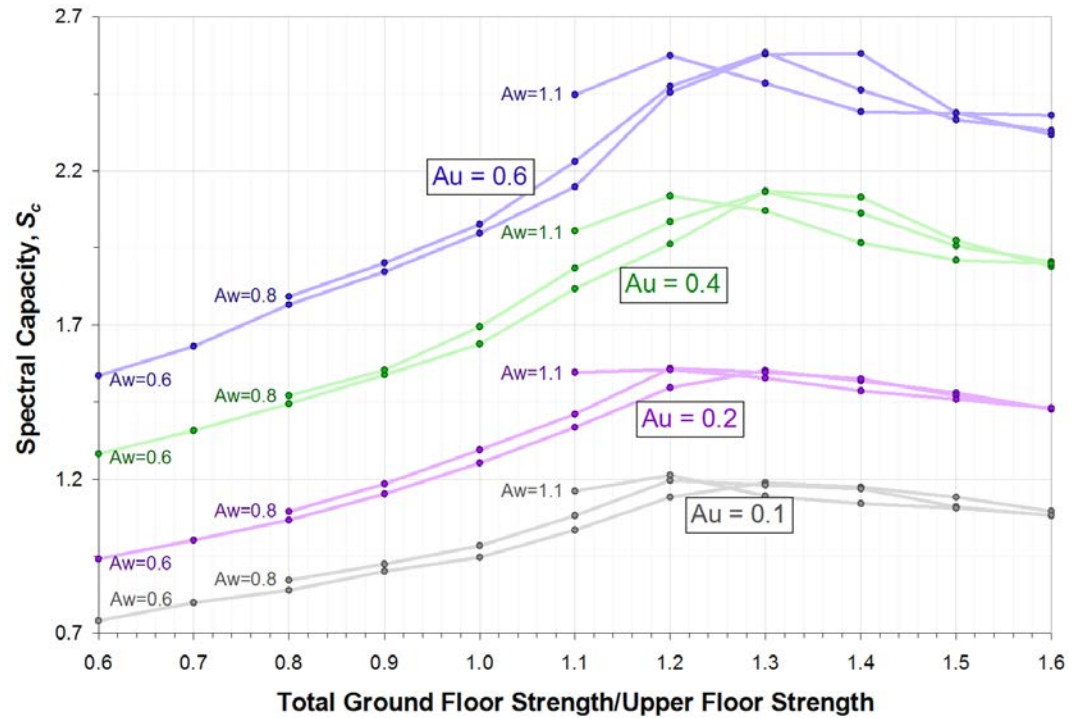
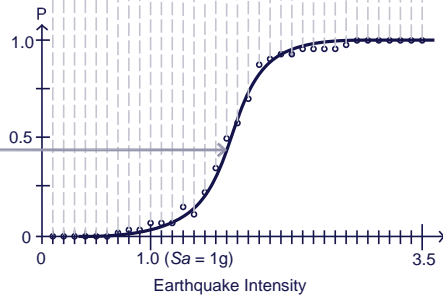
Time-history seed records:

(22) Bi-directional records = (44) individual  
Scaled so that median  $S_a(T = 0.3 \text{ sec}) = 1.0g$

(35) intensities per seed record varying from 0.1 to 3.5 by 0.1

Recover peak interstory drift ratios for each analysis

Given drift criteria, fit log-normal CDF

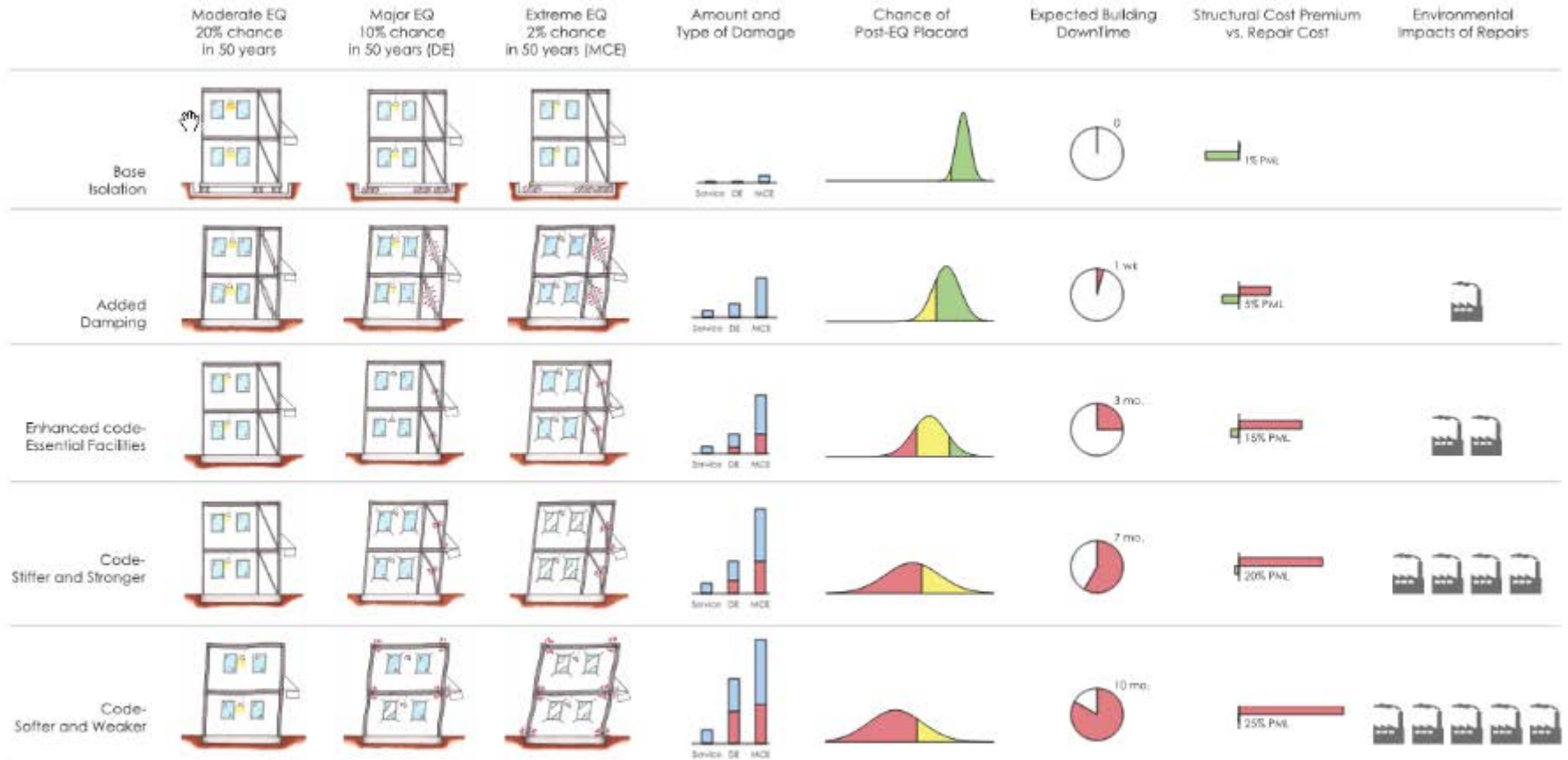






# UNDERSTANDING PERFORMANCE-BASED DESIGN

## Information for Smart Design Decisions



Earthquake damage for code-compliant buildings varies depending upon the level of shaking experienced and the characteristics of the building's structural system.

Damage to non-structural components, which can be more costly and disruptive than damage to the structure, can be measured and managed.

The odds of getting a green tag (safe), yellow tag (restricted), or red tag (unsafe) vary based on design choices.

Design choices affect the amount of time required before a building can be occupied after an earthquake.

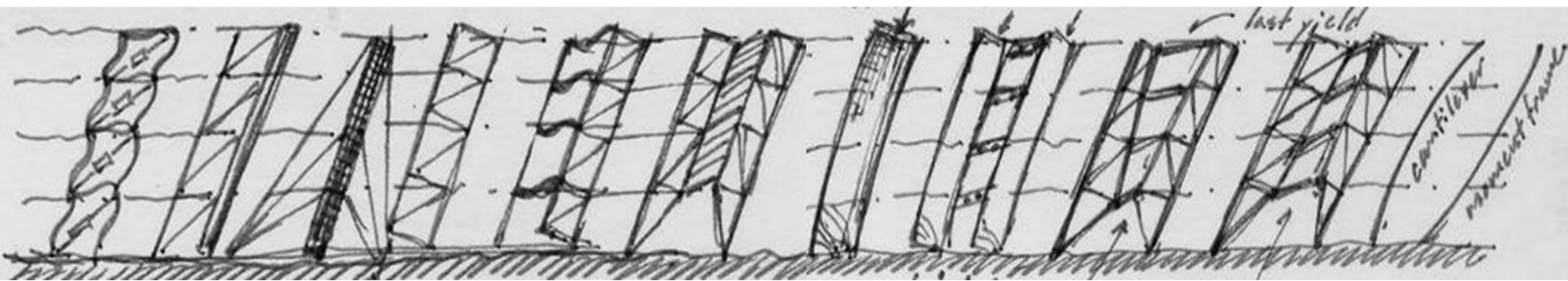
The red bar represents PNL (probable maximum loss). It is a measure of the repair cost as a percentage of building replacement cost.

The materials and work required for post-earthquake repair have environmental consequences that can be measured.

### Design Decisions Affect How Earthquakes Impact New Code-Compliant Buildings

The FEMA P-58 methodology can help inform decisions by calculating expected dollar losses, repair time, chances of receiving an unsafe placard, casualties, environmental impacts, and the uncertainty of each. See [www.fema.gov/P58](http://www.fema.gov/P58) for more information.

design choices are



**P e r f o r m a n c e   I n v e s t m e n t s**